

**(E)-N-[(E)-2-[(3,5-Dimethylbiphenyl-4-yl)imino]acenaphthen-1-ylidene]-2,6-dimethyl-4-phenylaniline**

Jianchao Yuan,\* Xiaoli Xie, Yufeng Liu, Chengping Miao and Jing Li

Key Laboratory of Eco-Environment-Related Polymer Materials of the Ministry of Education, Key Laboratory of Polymer Materials of Gansu Province, College of Chemistry & Chemical Engineering, Northwest Normal University, Lanzhou 730070, People's Republic of China

Correspondence e-mail: jianchaoyuan@nwnu.edu.cn

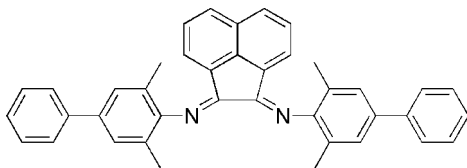
Received 14 November 2011; accepted 15 December 2011

Key indicators: single-crystal X-ray study;  $T = 296$  K; mean  $\sigma(\text{C}-\text{C}) = 0.006$  Å;  $R$  factor = 0.059;  $wR$  factor = 0.211; data-to-parameter ratio = 14.8.

The title compound,  $\text{C}_{40}\text{H}_{32}\text{N}_2$ , has crystallographic twofold rotation symmetry, with two C atoms lying on the axis. The dihedral angle between the two benzene rings of the 4-phenyl-2,6-dimethylphenyl group is  $35.74$  (17)°. The acenaphthene ring makes an angle of  $76.93$  (11)° with the benzene ring bonded to the N atom and an angle of  $41.53$  (13)° with the other benzene ring.

**Related literature**

The title compound was synthesized as an  $\alpha$ -diimine ligand for use in  $\text{Ni}^{\text{II}}$ - $\alpha$ -diimine olefin polymerization catalysts. For applications of metal-organic polymerization catalysts, see: Johnson *et al.* (1995); Killian *et al.* (1996); Popeney *et al.* (2005, 2010, 2011). For a related structure, see: Lohr *et al.* (2011).

**Experimental***Crystal data*

|  |                                   |
|--|-----------------------------------|
| $\text{C}_{40}\text{H}_{32}\text{N}_2$ | $V = 3082$ (4) Å <sup>3</sup>     |
| $M_r = 540.68$                         | $Z = 4$                           |
| Monoclinic, $C2/c$                     | Mo $K\alpha$ radiation            |
| $a = 22.994$ (14) Å                    | $\mu = 0.07$ mm <sup>-1</sup>     |
| $b = 8.676$ (5) Å                      | $T = 296$ K                       |
| $c = 18.652$ (18) Å                    | $0.23 \times 0.21 \times 0.19$ mm |
| $\beta = 124.084$ (4)°                 |                                   |

*Data collection*

|  |  |
|--|--|
| Bruker APEXII CCD diffractometer                             | 10667 measured reflections             |
| Absorption correction: multi-scan (SADABS; Sheldrick, 2008a) | 2857 independent reflections           |
| $T_{\text{min}} = 0.985$ , $T_{\text{max}} = 0.987$          | 1596 reflections with $I > 2\sigma(I)$ |
|  | $R_{\text{int}} = 0.031$               |

*Refinement*

|                                 |   |
|---------------------------------|---|
| $R[F^2 > 2\sigma(F^2)] = 0.059$ | 193 parameters                                      |
| $wR(F^2) = 0.211$               | H-atom parameters constrained                       |
| $S = 1.16$                      | $\Delta\rho_{\text{max}} = 0.23$ e Å <sup>-3</sup>  |
| 2857 reflections                | $\Delta\rho_{\text{min}} = -0.20$ e Å <sup>-3</sup> |

Data collection: APEX2 (Bruker, 2008); cell refinement: SAINT (Bruker, 2008); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008b); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008b); molecular graphics: SHELXTL (Sheldrick, 2008b); software used to prepare material for publication: SHELXTL.

We thank the National Natural Science Foundation of China (20964003) for funding. We also thank the Key Laboratory of Eco Environment-Related Polymer Materials of the Ministry of Education, Key Laboratory of Polymer Materials of Gansu Province (Northwest Normal University), for financial support.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: FY2034).

**References**

- Bruker (2008). SAINT and APEX2. Bruker AXS Inc., Madison, Wisconsin, USA.
- Johnson, L. K., Killian, C. M. & Brookhart, M. (1995). *J. Am. Chem. Soc.* **117**, 6414–6415.
- Killian, C. M., Tempel, D. J., Johnson, L. K. & Brookhart, M. (1996). *J. Am. Chem. Soc.* **118**, 11664–11665.
- Lohr, T. L., Piers, W. E. & Parvez, M. (2011). *Acta Cryst.* **E67**, o2280.
- Popeney, C. & Guan, Z. B. (2005). *Organometallics*, **24**, 1145–1155.
- Popeney, C. S. & Guan, Z. B. (2010). *Macromolecules*, **43**, 4091–4097.
- Popeney, C. S., Levins, C. M. & Guan, Z. B. (2011). *Organometallics*, **30**, 2432–2452.
- Sheldrick, G. M. (2008a). SADABS. University of Göttingen, Germany.
- Sheldrick, G. M. (2008b). *Acta Cryst.* **A64**, 112–122.

**supplementary materials**

*Acta Cryst.* (2012). E68, o210 [ doi:10.1107/S1600536811054092 ]

**(*E*)-*N*-{(*E*)-2-[(3,5-Dimethylbiphenyl-4-yl)imino]acenaphthen-1-ylidene}-2,6-dimethyl-4-phenylaniline**

**J. Yuan, X. Xie, Y. Liu, C. Miao and J. Li**

**Comment**

In recent years,  $\alpha$ -diimine nickel catalysts have drawn wide-spread attention due to their high catalytic activity in ethylene polymerization (Johnson *et al.*, 1995; Killian *et al.*, 1996). It is well known that the ligand structure has significant influence on the product properties and polymerization activities (Popeney *et al.*, 2011; Popeney *et al.*, 2010; Popeney *et al.*, 2005). In this study, we designed and synthesized the title compound as a bidentate ligand, and its molecular structure was characterized by X-ray diffraction.

**Experimental**

Formic acid (1 ml) was added to a stirred solution of acenaphthenequinone (0.25 g, 1.37 mmol) and 4-phenyl-2,6-dimethylaniline (0.54 g, 2.74 mmol) in methanol (20 ml). The mixture was refluxed for 24 h, then cooled and the precipitate was separated by filtration. The solid was recrystallized from ethanol/dichloromethane ( $v/v = 8:1$ ), washed and dried under vacuum. Yield: 0.55 g (74%). Anal. Calcd. for  $C_{40}H_{32}N_2$ : C, 88.85; H, 5.97; N, 5.18. Found: C, 88.91; H, 6.03; N, 5.06. Crystals suitable for X-ray structure determination were grown from a solution of the title compound in a mixture of cyclohexane/dichloromethane (1:2,  $v/v$ ) by slow evaporation.

**Refinement**

All hydrogen atoms were placed in calculated positions with C—H distances of 0.93 and 0.96 Å for aryl and methyl type H-atoms, respectively. They were included in the refinement in a riding model approximation. The H-atoms were assigned  $U_{iso} = 1.2$  times  $U_{eq}$  of the aryl C atoms and 1.5 times  $U_{eq}$  of the methyl C atoms.

**Figures**

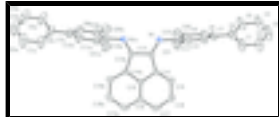


Fig. 1. Structure of the title compound, with displacement ellipsoids drawn at the 30% probability level. H-atoms have been excluded for clarity. The atom name suffix indicates symmetry code (a):  $-x, y, -z + 1/2$ .

**(*E*)-*N*-{(*E*)-2-[(3,5-Dimethylbiphenyl-4-yl)imino]acenaphthen-1-ylidene}-2,6-dimethyl-4-phenylaniline**

*Crystal data*

$C_{40}H_{32}N_2$

$M_r = 540.68$

Monoclinic,  $C2/c$

$a = 22.994$  (14) Å

$F(000) = 1144$

$D_x = 1.165$  Mg m $^{-3}$

Mo  $K\alpha$  radiation,  $\lambda = 0.71073$  Å

Cell parameters from 3073 reflections

# supplementary materials

---

|                               |   |
|-------------------------------|---|
| $b = 8.676 (5) \text{ \AA}$   | $\theta = 2.1\text{--}25.7^\circ$         |
| $c = 18.652 (18) \text{ \AA}$ | $\mu = 0.07 \text{ mm}^{-1}$              |
| $\beta = 124.084 (4)^\circ$   | $T = 296 \text{ K}$                       |
| $V = 3082 (4) \text{ \AA}^3$  | Block, red                                |
| $Z = 4$                       | $0.23 \times 0.21 \times 0.19 \text{ mm}$ |

## Data collection

|  |  |
|--|--|
| Bruker APEXII CCD diffractometer                             | 2857 independent reflections   |
| Radiation source: fine-focus sealed tube graphite            | 1596 reflections with $I > 2\sigma(I)$                                 |
| $\varphi$ and $\omega$ scans                                 | $R_{\text{int}} = 0.031$   |
| Absorption correction: multi-scan (SADABS; Sheldrick, 2008a) | $\theta_{\text{max}} = 25.5^\circ$ , $\theta_{\text{min}} = 2.1^\circ$ |
| $T_{\text{min}} = 0.985$ , $T_{\text{max}} = 0.987$          | $h = -27 \rightarrow 27$   |
| 10667 measured reflections                                   | $k = -10 \rightarrow 10$   |
|  | $l = -22 \rightarrow 20$   |

## Refinement

|                                 |  |
|---------------------------------|--|
| Refinement on $F^2$             | Primary atom site location: structure-invariant direct methods |
| Least-squares matrix: full      | Secondary atom site location: difference Fourier map           |
| $R[F^2 > 2\sigma(F^2)] = 0.059$ | Hydrogen site location: inferred from neighbouring sites       |
| $wR(F^2) = 0.211$               | H-atom parameters constrained                                  |
| $S = 1.16$                      | $w = 1/[\sigma^2(F_o^2) + (0.0705P)^2 + 3.4006P]$              |
| 2857 reflections                | where $P = (F_o^2 + 2F_c^2)/3$                                 |
| 193 parameters                  | $(\Delta/\sigma)_{\text{max}} < 0.001$                         |
| 0 restraints                    | $\Delta\rho_{\text{max}} = 0.23 \text{ e \AA}^{-3}$            |
|                                 | $\Delta\rho_{\text{min}} = -0.20 \text{ e \AA}^{-3}$           |

## Special details

**Geometry.** All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement.** Refinement of  $F^2$  against ALL reflections. The weighted  $R$ -factor  $wR$  and goodness of fit  $S$  are based on  $F^2$ , conventional  $R$ -factors  $R$  are based on  $F$ , with  $F$  set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating  $R$ -factors(gt) etc. and is not relevant to the choice of reflections for refinement.  $R$ -factors based on  $F^2$  are statistically about twice as large as those based on  $F$ , and  $R$ -factors based on ALL data will be even larger.

## Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters ( $\text{\AA}^2$ )

|    | $x$        | $y$        | $z$        | $U_{\text{iso}}^*/U_{\text{eq}}$ |
|----|------------|------------|------------|----------------------------------|
| C1 | 0.2760 (2) | 0.8437 (6) | 0.7549 (2) | 0.1024 (15)                      |

|      |              |            |              |             |
|------|--------------|------------|--------------|-------------|
| H1   | 0.2411       | 0.7699     | 0.7368       | 0.123*      |
| C2   | 0.3295 (3)   | 0.8543 (8) | 0.8419 (3)   | 0.132 (2)   |
| H2   | 0.3303       | 0.7877     | 0.8815       | 0.159*      |
| C3   | 0.3807 (3)   | 0.9614 (9) | 0.8696 (3)   | 0.135 (3)   |
| H3   | 0.4158       | 0.9705     | 0.9283       | 0.162*      |
| C4   | 0.3807 (2)   | 1.0559 (8) | 0.8112 (4)   | 0.126 (2)   |
| H4   | 0.4165       | 1.1278     | 0.8300       | 0.151*      |
| C5   | 0.3271 (2)   | 1.0452 (6) | 0.7229 (3)   | 0.1089 (16) |
| H5   | 0.3277       | 1.1089     | 0.6832       | 0.131*      |
| C6   | 0.27359 (18) | 0.9396 (5) | 0.6951 (2)   | 0.0804 (11) |
| C7   | 0.21565 (18) | 0.9254 (4) | 0.6012 (2)   | 0.0691 (9)  |
| C8   | 0.22787 (19) | 0.9461 (4) | 0.5373 (2)   | 0.0719 (10) |
| H8   | 0.2729       | 0.9726     | 0.5534       | 0.086*      |
| C9   | 0.1758 (2)   | 0.9289 (4) | 0.4504 (2)   | 0.0707 (10) |
| C10  | 0.10860 (19) | 0.8859 (3) | 0.42739 (19) | 0.0639 (9)  |
| C11  | 0.09402 (17) | 0.8687 (4) | 0.4894 (2)   | 0.0668 (9)  |
| C12  | 0.14776 (18) | 0.8885 (4) | 0.5757 (2)   | 0.0720 (10) |
| H12  | 0.1382       | 0.8768     | 0.6177       | 0.086*      |
| C13  | 0.02861 (17) | 0.7530 (3) | 0.29823 (18) | 0.0617 (9)  |
| C14  | 0.04351 (15) | 0.5886 (3) | 0.32523 (18) | 0.0526 (8)  |
| C15  | 0.0000       | 0.5015 (4) | 0.2500       | 0.0497 (10) |
| C16  | 0.0000       | 0.3396 (5) | 0.2500       | 0.0642 (12) |
| C17  | 0.0457 (2)   | 0.2681 (4) | 0.3300 (2)   | 0.0833 (12) |
| H17  | 0.0476       | 0.1610     | 0.3334       | 0.100*      |
| C18  | 0.08782 (19) | 0.3537 (4) | 0.4034 (2)   | 0.0753 (10) |
| H18  | 0.1177       | 0.3028     | 0.4555       | 0.090*      |
| C19  | 0.08738 (16) | 0.5154 (3) | 0.4025 (2)   | 0.0619 (9)  |
| H19  | 0.1162       | 0.5712     | 0.4532       | 0.074*      |
| C20  | 0.1907 (3)   | 0.9524 (5) | 0.3822 (2)   | 0.1042 (15) |
| H20A | 0.2376       | 0.9908     | 0.4088       | 0.156*      |
| H20B | 0.1579       | 1.0253     | 0.3402       | 0.156*      |
| H20C | 0.1861       | 0.8559     | 0.3542       | 0.156*      |
| C21  | 0.02117 (19) | 0.8275 (5) | 0.4649 (3)   | 0.0984 (14) |
| H21A | -0.0123      | 0.8974     | 0.4212       | 0.148*      |
| H21B | 0.0194       | 0.8350     | 0.5151       | 0.148*      |
| H21C | 0.0101       | 0.7240     | 0.4430       | 0.148*      |
| N1   | 0.05454 (16) | 0.8787 (3) | 0.33777 (16) | 0.0755 (9)  |

Atomic displacement parameters ( $\text{\AA}^2$ )

|    | $U^{11}$  | $U^{22}$  | $U^{33}$  | $U^{12}$     | $U^{13}$    | $U^{23}$     |
|----|-----------|-----------|-----------|--------------|-------------|--------------|
| C1 | 0.081 (3) | 0.157 (4) | 0.056 (2) | 0.001 (3)    | 0.030 (2)   | -0.013 (3)   |
| C2 | 0.095 (3) | 0.217 (7) | 0.060 (3) | 0.012 (4)    | 0.028 (3)   | -0.017 (3)   |
| C3 | 0.071 (3) | 0.239 (7) | 0.071 (3) | 0.023 (4)    | 0.025 (3)   | -0.055 (4)   |
| C4 | 0.070 (3) | 0.205 (6) | 0.098 (4) | -0.027 (3)   | 0.044 (3)   | -0.082 (4)   |
| C5 | 0.080 (3) | 0.158 (5) | 0.082 (3) | -0.031 (3)   | 0.041 (2)   | -0.059 (3)   |
| C6 | 0.064 (2) | 0.113 (3) | 0.060 (2) | -0.005 (2)   | 0.0321 (19) | -0.030 (2)   |
| C7 | 0.070 (2) | 0.074 (2) | 0.054 (2) | -0.0068 (17) | 0.0291 (18) | -0.0192 (17) |

## supplementary materials

---

|     |             |             |             |              |             |              |
|-----|-------------|-------------|-------------|--------------|-------------|--------------|
| C8  | 0.077 (2)   | 0.070 (2)   | 0.063 (2)   | -0.0172 (18) | 0.0356 (19) | -0.0174 (17) |
| C9  | 0.095 (3)   | 0.0485 (18) | 0.058 (2)   | -0.0117 (18) | 0.036 (2)   | -0.0076 (15) |
| C10 | 0.084 (2)   | 0.0305 (15) | 0.0465 (19) | 0.0000 (15)  | 0.0174 (18) | -0.0051 (12) |
| C11 | 0.063 (2)   | 0.0528 (19) | 0.060 (2)   | -0.0019 (15) | 0.0198 (17) | -0.0129 (15) |
| C12 | 0.067 (2)   | 0.082 (2)   | 0.059 (2)   | -0.0036 (18) | 0.0293 (18) | -0.0152 (17) |
| C13 | 0.080 (2)   | 0.0283 (15) | 0.0504 (17) | -0.0004 (14) | 0.0208 (16) | -0.0002 (12) |
| C14 | 0.0646 (18) | 0.0322 (15) | 0.0498 (17) | 0.0021 (13)  | 0.0252 (15) | 0.0007 (12)  |
| C15 | 0.063 (2)   | 0.0282 (19) | 0.051 (2)   | 0.000        | 0.027 (2)   | 0.000        |
| C16 | 0.078 (3)   | 0.036 (2)   | 0.064 (3)   | 0.000        | 0.031 (3)   | 0.000        |
| C17 | 0.102 (3)   | 0.0344 (17) | 0.087 (3)   | 0.0073 (17)  | 0.036 (2)   | 0.0108 (17)  |
| C18 | 0.086 (2)   | 0.050 (2)   | 0.065 (2)   | 0.0111 (17)  | 0.0268 (19) | 0.0197 (17)  |
| C19 | 0.073 (2)   | 0.0420 (17) | 0.0547 (19) | 0.0052 (15)  | 0.0257 (17) | 0.0054 (14)  |
| C20 | 0.145 (4)   | 0.091 (3)   | 0.073 (3)   | -0.020 (3)   | 0.059 (3)   | 0.001 (2)    |
| C21 | 0.067 (2)   | 0.105 (3)   | 0.091 (3)   | -0.003 (2)   | 0.025 (2)   | -0.028 (2)   |
| N1  | 0.100 (2)   | 0.0295 (13) | 0.0510 (16) | -0.0021 (13) | 0.0140 (15) | -0.0045 (11) |

### *Geometric parameters (Å, °)*

|          |           |                           |             |
|----------|-----------|---------------------------|-------------|
| C1—C6    | 1.368 (6) | C12—H12                   | 0.9300      |
| C1—C2    | 1.386 (6) | C13—N1                    | 1.263 (4)   |
| C1—H1    | 0.9300    | C13—C14                   | 1.487 (4)   |
| C2—C3    | 1.355 (8) | C13—C13 <sup>i</sup>      | 1.522 (6)   |
| C2—H2    | 0.9300    | C14—C19                   | 1.368 (4)   |
| C3—C4    | 1.363 (8) | C14—C15                   | 1.403 (3)   |
| C3—H3    | 0.9300    | C15—C14 <sup>i</sup>      | 1.403 (3)   |
| C4—C5    | 1.402 (6) | C15—C16                   | 1.404 (6)   |
| C4—H4    | 0.9300    | C16—C17 <sup>i</sup>      | 1.400 (4)   |
| C5—C6    | 1.381 (6) | C16—C17                   | 1.400 (4)   |
| C5—H5    | 0.9300    | C17—C18                   | 1.370 (5)   |
| C6—C7    | 1.497 (5) | C17—H17                   | 0.9300      |
| C7—C8    | 1.381 (5) | C18—C19                   | 1.403 (4)   |
| C7—C12   | 1.391 (5) | C18—H18                   | 0.9300      |
| C8—C9    | 1.382 (4) | C19—H19                   | 0.9300      |
| C8—H8    | 0.9300    | C20—H20A                  | 0.9600      |
| C9—C10   | 1.404 (5) | C20—H20B                  | 0.9600      |
| C9—C20   | 1.504 (5) | C20—H20C                  | 0.9600      |
| C10—C11  | 1.381 (5) | C21—H21A                  | 0.9600      |
| C10—N1   | 1.419 (4) | C21—H21B                  | 0.9600      |
| C11—C12  | 1.385 (4) | C21—H21C                  | 0.9600      |
| C11—C21  | 1.512 (5) |                           |             |
| C6—C1—C2 | 121.2 (5) | C7—C12—H12                | 119.2       |
| C6—C1—H1 | 119.4     | N1—C13—C14                | 133.3 (3)   |
| C2—C1—H1 | 119.4     | N1—C13—C13 <sup>i</sup>   | 120.18 (17) |
| C3—C2—C1 | 120.3 (6) | C14—C13—C13 <sup>i</sup>  | 106.44 (15) |
| C3—C2—H2 | 119.9     | C19—C14—C15               | 119.7 (3)   |
| C1—C2—H2 | 119.9     | C19—C14—C13               | 134.2 (3)   |
| C2—C3—C4 | 119.8 (5) | C15—C14—C13               | 106.2 (2)   |
| C2—C3—H3 | 120.1     | C14 <sup>i</sup> —C15—C14 | 114.8 (3)   |

|                |            |  |             |
|----------------|------------|--|-------------|
| C4—C3—H3       | 120.1      | C14 <sup>i</sup> —C15—C16                  | 122.62 (17) |
| C3—C4—C5       | 120.4 (5)  | C14—C15—C16                                | 122.62 (17) |
| C3—C4—H4       | 119.8      | C17 <sup>i</sup> —C16—C17                  | 127.3 (4)   |
| C5—C4—H4       | 119.8      | C17 <sup>i</sup> —C16—C15                  | 116.3 (2)   |
| C6—C5—C4       | 119.8 (5)  | C17—C16—C15                                | 116.3 (2)   |
| C6—C5—H5       | 120.1      | C18—C17—C16                                | 120.8 (3)   |
| C4—C5—H5       | 120.1      | C18—C17—H17                                | 119.6       |
| C1—C6—C5       | 118.5 (4)  | C16—C17—H17                                | 119.6       |
| C1—C6—C7       | 120.4 (4)  | C17—C18—C19                                | 122.3 (3)   |
| C5—C6—C7       | 121.1 (4)  | C17—C18—H18                                | 118.8       |
| C8—C7—C12      | 117.9 (3)  | C19—C18—H18                                | 118.8       |
| C8—C7—C6       | 121.4 (3)  | C14—C19—C18                                | 118.2 (3)   |
| C12—C7—C6      | 120.8 (3)  | C14—C19—H19                                | 120.9       |
| C9—C8—C7       | 122.5 (3)  | C18—C19—H19                                | 120.9       |
| C9—C8—H8       | 118.7      | C9—C20—H20A                                | 109.5       |
| C7—C8—H8       | 118.7      | C9—C20—H20B                                | 109.5       |
| C8—C9—C10      | 117.9 (3)  | H20A—C20—H20B                              | 109.5       |
| C8—C9—C20      | 121.3 (4)  | C9—C20—H20C                                | 109.5       |
| C10—C9—C20     | 120.8 (3)  | H20A—C20—H20C                              | 109.5       |
| C11—C10—C9     | 121.0 (3)  | H20B—C20—H20C                              | 109.5       |
| C11—C10—N1     | 121.2 (3)  | C11—C21—H21A                               | 109.5       |
| C9—C10—N1      | 117.3 (3)  | C11—C21—H21B                               | 109.5       |
| C10—C11—C12    | 118.9 (3)  | H21A—C21—H21B                              | 109.5       |
| C10—C11—C21    | 121.4 (3)  | C11—C21—H21C                               | 109.5       |
| C12—C11—C21    | 119.7 (4)  | H21A—C21—H21C                              | 109.5       |
| C11—C12—C7     | 121.7 (3)  | H21B—C21—H21C                              | 109.5       |
| C11—C12—H12    | 119.2      | C13—N1—C10                                 | 122.7 (2)   |
| C6—C1—C2—C3    | 0.3 (8)    | C21—C11—C12—C7                             | 179.6 (3)   |
| C1—C2—C3—C4    | -2.0 (8)   | C8—C7—C12—C11                              | 1.7 (5)     |
| C2—C3—C4—C5    | 1.5 (8)    | C6—C7—C12—C11                              | -177.3 (3)  |
| C3—C4—C5—C6    | 0.8 (7)    | N1—C13—C14—C19                             | 4.2 (7)     |
| C2—C1—C6—C5    | 2.0 (7)    | C13 <sup>i</sup> —C13—C14—C19              | -178.1 (4)  |
| C2—C1—C6—C7    | 179.5 (4)  | N1—C13—C14—C15                             | -176.1 (4)  |
| C4—C5—C6—C1    | -2.5 (6)   | C13 <sup>i</sup> —C13—C14—C15              | 1.6 (4)     |
| C4—C5—C6—C7    | 180.0 (4)  | C19—C14—C15—C14 <sup>i</sup>               | 179.1 (3)   |
| C1—C6—C7—C8    | -142.6 (4) | C13—C14—C15—C14 <sup>i</sup>               | -0.65 (17)  |
| C5—C6—C7—C8    | 34.9 (5)   | C19—C14—C15—C16                            | -0.9 (3)    |
| C1—C6—C7—C12   | 36.4 (5)   | C13—C14—C15—C16                            | 179.35 (17) |
| C5—C6—C7—C12   | -146.1 (4) | C14 <sup>i</sup> —C15—C16—C17 <sup>i</sup> | 0.5 (2)     |
| C12—C7—C8—C9   | -1.1 (5)   | C14—C15—C16—C17 <sup>i</sup>               | -179.5 (2)  |
| C6—C7—C8—C9    | 177.9 (3)  | C14 <sup>i</sup> —C15—C16—C17              | -179.5 (2)  |
| C7—C8—C9—C10   | -1.3 (5)   | C14—C15—C16—C17                            | 0.5 (2)     |
| C7—C8—C9—C20   | 179.9 (3)  | C17 <sup>i</sup> —C16—C17—C18              | 179.8 (4)   |
| C8—C9—C10—C11  | 3.2 (5)    | C15—C16—C17—C18                            | -0.2 (4)    |
| C20—C9—C10—C11 | -178.0 (3) | C16—C17—C18—C19                            | 0.1 (6)     |
| C8—C9—C10—N1   | 175.9 (3)  | C15—C14—C19—C18                            | 0.8 (5)     |

## supplementary materials

---

|                |            |                              |            |
|----------------|------------|------------------------------|------------|
| C20—C9—C10—N1  | -5.3 (5)   | C13—C14—C19—C18              | -179.5 (4) |
| C9—C10—C11—C12 | -2.7 (5)   | C17—C18—C19—C14              | -0.5 (6)   |
| N1—C10—C11—C12 | -175.1 (3) | C14—C13—N1—C10               | -1.7 (7)   |
| C9—C10—C11—C21 | 177.9 (3)  | C13 <sup>i</sup> —C13—N1—C10 | -179.2 (4) |
| N1—C10—C11—C21 | 5.5 (5)    | C11—C10—N1—C13               | -78.7 (5)  |
| C10—C11—C12—C7 | 0.2 (5)    | C9—C10—N1—C13                | 108.6 (4)  |

Symmetry codes: (i)  $-x, y, -z+1/2$ .



Fig. 1

